T A S A C

A Computer Program for

Thermal Analysis of Severe Accident Conditions

Version 3/01, Dec. 1991.

Model Description and User's Guide



M.Stempniewicz, P.Marks, K.Salwa Institute of Atomic Energy PL-05-400 Otwock, Swierk

ABSTRACT

TASAC (Thermal Analysis of Severe Accident Conditions) is a computer program developed in the Institute of Atomic Energy, written in FORTRAN 77 for the digital computer analysis of PWR rod bundle during severe accident conditions.

The program has the ability to model an early stage of core degradation including heat transfer inside the rods, convective and radiative heat exchange as well as cladding interaction with coolant and fuel, hydrogen generation, melting, relocations and refreezing of fuel rod materials with dissolution of UO_2 and ZrO_2 in liquid phase.

The code was applied for the simulation of International Standard Problem number 28 (ISP-28), performed on PHEBUS test facility. This report contains the program physical models description, detailed description of input data requirements and results of code verification. The main directions for future code development are formulated.

CONTENTS

1. ABSTRACT	1-1
2. INTRODUCTION	2-1
3. TASAC PHYSICAL MODELS. 3.1. Conduction in solids. 3.2. Radiation heat transfer. 3.3. Fluid transport, convective heat transfer. 3.4. Friction factor model. 3.5. Gap conductance. 3.6. Zircaloy oxidation. 3.7. UO2 and ZrO2 dissolution by molten Zr. 3.8. Relocation model. 3.9. Built-in material properties.	3-1 3-4 3-6 3-9 3-12 3-14 3-16 3-19 3-24
<pre>4. COMPUTER PROGRAM DESCRIPTION</pre>	4-1 4-1 4-5
5. USE OF TASAC. 5.1. Input data description. 5.2. Output data description.	5-1 5-1 5-15
 6. CODE VERIFICATION. 6.1. Verification of independent models. 6.2. Sensitivity study. 6.3. Empirical verification - comparison with 	6-1 6-1 6-9
PHEBUS B9+ experiment	6-17
<pre>7. CONCLUSIONS, FUTURE DEVELOPMENT</pre>	7-1 8-1

LIST OF FIGURES

Fig.3.1.1.	Conductor geometry	3-2
Fig.3.1.2.	Fuel and cladding meshing	3-4
Fig.3.3.1.	Fluid channel axial subsection	3-7
Fig.3.4.1.	Comparison of friction factors for the Colebrook	
5	and TASAC friction factor models.	3-11
Fig.3.7.1.1.	Comparison of theoretical equation of Kim-Olander	
	dissolution model with experimental curve.	3-17
Fig.3.7.1.2.	UO2 dissolution.	3-18
Fig. 3. 8.1.	Relocating Laver - definitions and symbols.	3-20
Fig. 4.1.1.	TASAC 3/01 general organization.	4-2
Fig 4 1 2	STDY - Steady state calculations organization	4-2
Fig 4 1 3	TRAN - Transient calculations organization	4-3
Fig 4 1 4	HEAT - Subroutine organization	<u> </u>
Fig. 5.2.1	Example of a single edit of the TASAC code	5-18
Fig. 6.1.1	Time of freezing of culinder	6_1
Fig. 0.1.1.	Time of freezing of cyrinder	6-3
Fig.0.1.2.	Zi oxidation. External reaction	6 1
Fig. 6.1.3.	Zr oxidation. Internal reaction	6-4
F1g.6.1.4.	2r oxidation. Internal/external reaction	6-3
F1g.6.1.5.	2r oxidation. Internal/external reaction and	<i>c c</i>
	dissolution.	6-6
Fig.6.1.6.	Relocations. Small time step, explicit	6-7
Fig.6.1.7.	Relocations. Large time step, explicit	6-7
Fig.6.1.8.	Relocations. Small time step, implicit	6-8
Fig.6.1.9.	Relocations. Large time step, implicit	6-8
Fig.6.2.1.	Temperature prediction for different time steps	
	10 [s], and 500 [s]	6-10
Fig.6.2.2.	Temperature prediction for different time steps	
	10 [s], and 500 [s]	6-11
Fig.6.2.3.	Channel blockage prediction for time steps	
	10 s, and 500 s	6-12
Fig.6.2.4.	UO2 dissolution profile prediction for time steps	
	10 s, and 500 s	6-13
Fig.6.2.5.	Influence of flowdown velocity for channel	
	blockage profile	6-14
Fig.6.2.6.	Influence of flowdown velocity for UO2 diss	6-15
Fig.6.2.7.	Influence of convective heat transfer coeff.	
-	for channel blockage profile	6-16
Fig.6.2.8.	Influence of convective heat transfer coeff.	
	for UO2 dissolution profile	6-16
Fig.6.3.2.	PHEBUS B9+, rod No. 4 fuel temperature, 70 cm.	6-21
Fig.6.3.3.	PHEBUS B9+, rod No. 4 fuel temperature, 60 cm.	6-21
Fig 6 3 4	PHEBUS B9+, rod No. 2 clad temp , 20,40,50 cm	6-22
Fig 6 3 5	PHEBUS B9+, coolant outlet temperature	6-22
Fig 6 3 6	PHEBUS B9+, axial temperature profile	6-23
Fig 6 3 7	PHEBUS B9+, axial oxidation profile	6-23
y.u.u./. Fia 6 3 8	PHEBIIS B9+ hydrogen mass flux kg/s	6-21
y.0.3.0. Fia 6 3 9	PHEBIIS B9+ total hydrogen generation by	6-24
$F_{10} = 0.0000$	PHEBUS B9+ 1102 dissolution profile	6-25
$F_{1} = 0.0 \cdot 10.$	DUERNIG ROt channel blockage - avial profile	6-25
rry.v.j.tt.	INEROS DEF, CHANNET DIOCRAYE - AXIAI PIUIIIE	0-20